

Axisymmetric dynamo action is possible (with anisotropic conductivity)

“[...] things we thought impossible are possible.” (Axel B.)

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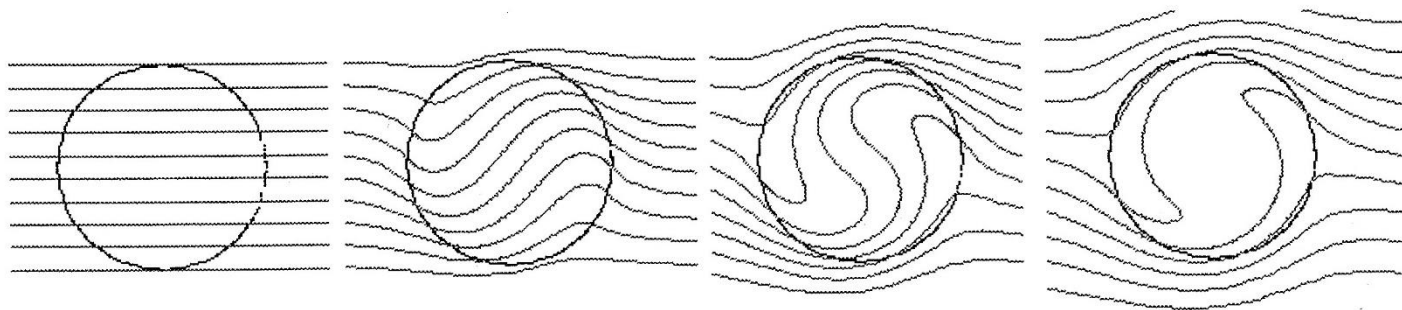
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Introduction

“[...] things we thought impossible ...”

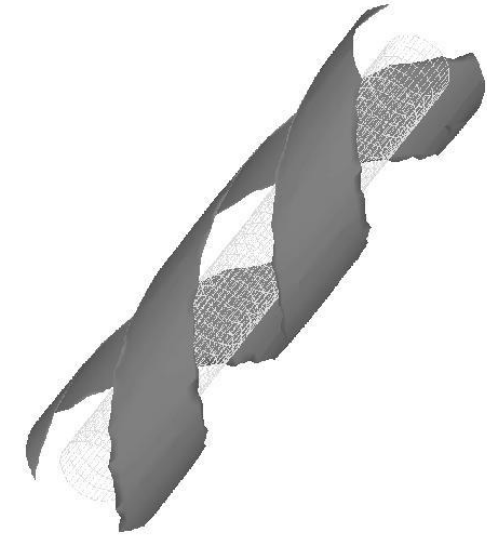
Dynamo action from **2D azimuthal shear** is impossible !



Parker (1966)

In addition, from **Cowling's theorem**, axisymmetric dynamo is impossible !

Helical shear
 \Rightarrow dynamo action

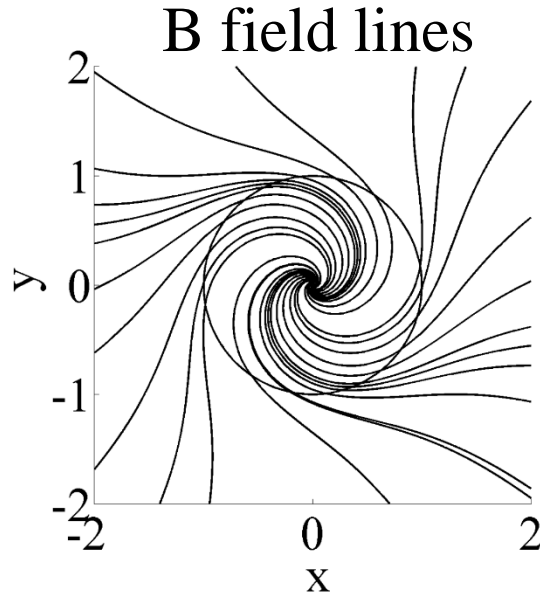


Ponomarenko (1973)

$m=1$

Introduction

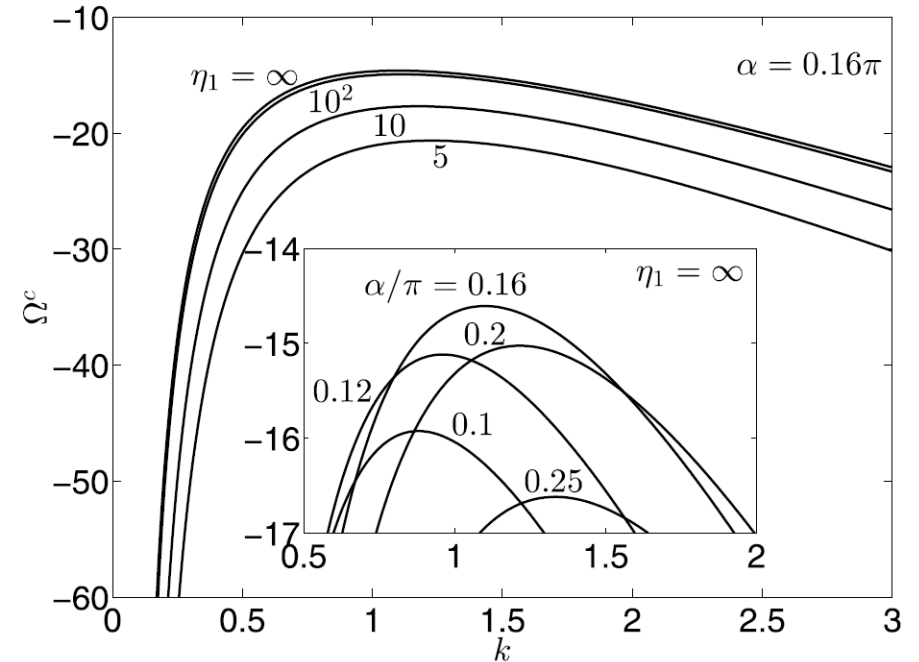
“[...] things we thought impossible ... are possible”



We will demonstrate that **2D azimuthal shear** can produce **axisymmetric dynamo** action, provided the electrical **conductivity is anisotropic**

Critical magnetic Reynolds number

$$\Omega^c = \frac{c}{s} (I_1(\tilde{k})K_1(\tilde{k}) - I_1(k)K_1(k))^{-1}$$



- 1. How can anisotropic conductivity beat Cowling's antidynamo theorem ?**
2. Exact solution of the induction equation
3. Conclusion and outlook

Cowling's antidynamo theorem (1934)

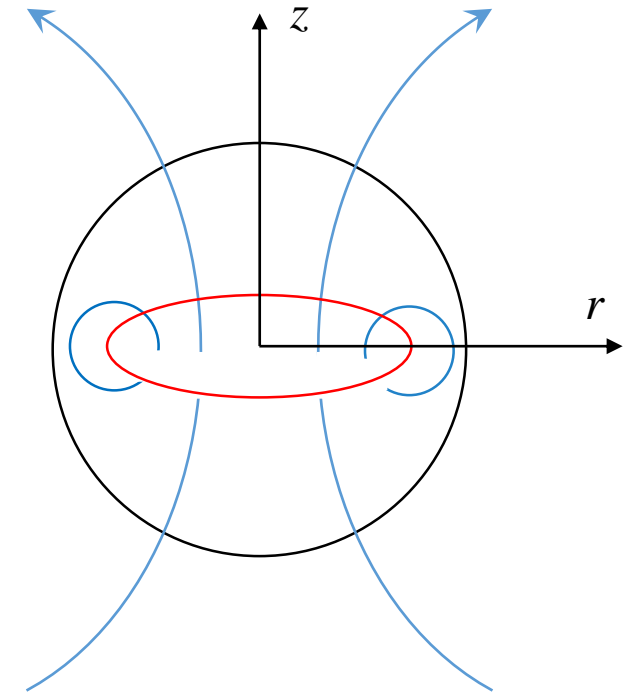
$$\partial_t \mathbf{B} = \nabla \times (\mathbf{u} \times \mathbf{B}) - \nabla \times \left(\frac{1}{\sigma} \nabla \times \left(\frac{\mathbf{B}}{\mu} \right) \right)$$

« An **axisymmetric magnetic field cannot** be generated by dynamo action under the assumption of **axisymmetry** of

- velocity field,
- electrical conductivity,
- magnetic permeability and
- shape of the conductor »

(Kaiser & Tilgner, 2014)

Cowling (1934)
Backus (1957)
Braginskii (1964)
Lortz (1968)
Moffatt (1978)
Ivers & James (1984)
Fearn (1988)
Proctor (2007)

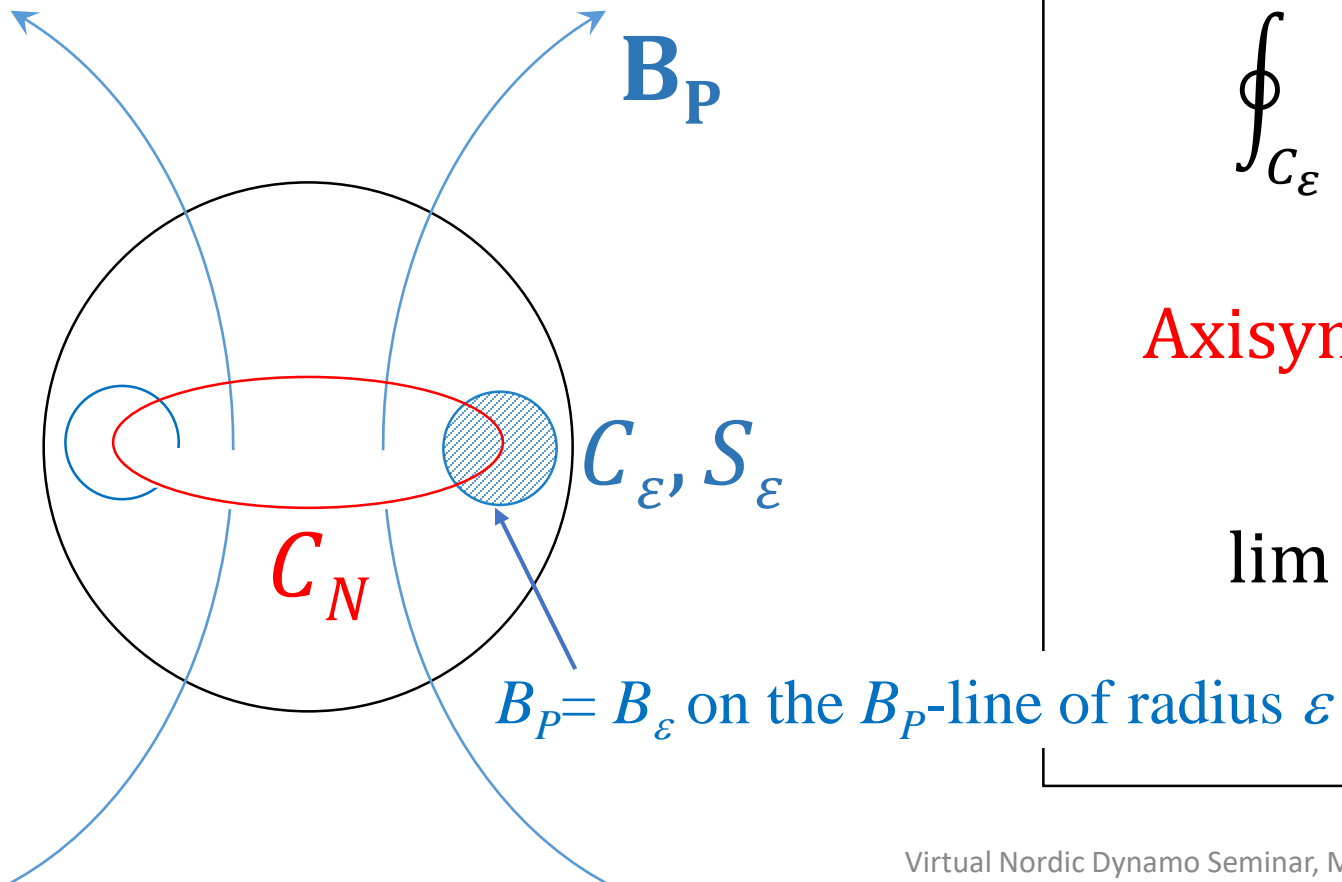


An axisymmetric world

Generalized to time-dependent / nonsolenoidal velocity, variable conductivity, ...

Cowling's neutral point argument

Poloidal / Toroidal decomposition



Assume \mathbf{B}_P

$$\mathbf{j}_T = \nabla \times \frac{\mathbf{B}_P}{\mu} = \sigma(\mathbf{E}_T + \mathbf{u}_P \times \mathbf{B}_P)$$

$$\oint_{C_\varepsilon} \frac{\mathbf{B}_P}{\mu} dl = \int_{S_\varepsilon} \sigma(\mathbf{E}_T + \underbrace{\mathbf{u}_P \times \mathbf{B}_P}_{\leq U_P B_\varepsilon}) \cdot d\mathbf{S}$$

Axisymmetry $\Rightarrow \mathbf{E}_T = 0$

$$\Rightarrow 2\pi\varepsilon \frac{B_\varepsilon}{\mu} \leq \sigma U_P B_\varepsilon \pi \varepsilon^2$$

$$\lim \varepsilon = 0 \Rightarrow B_\varepsilon = 0$$

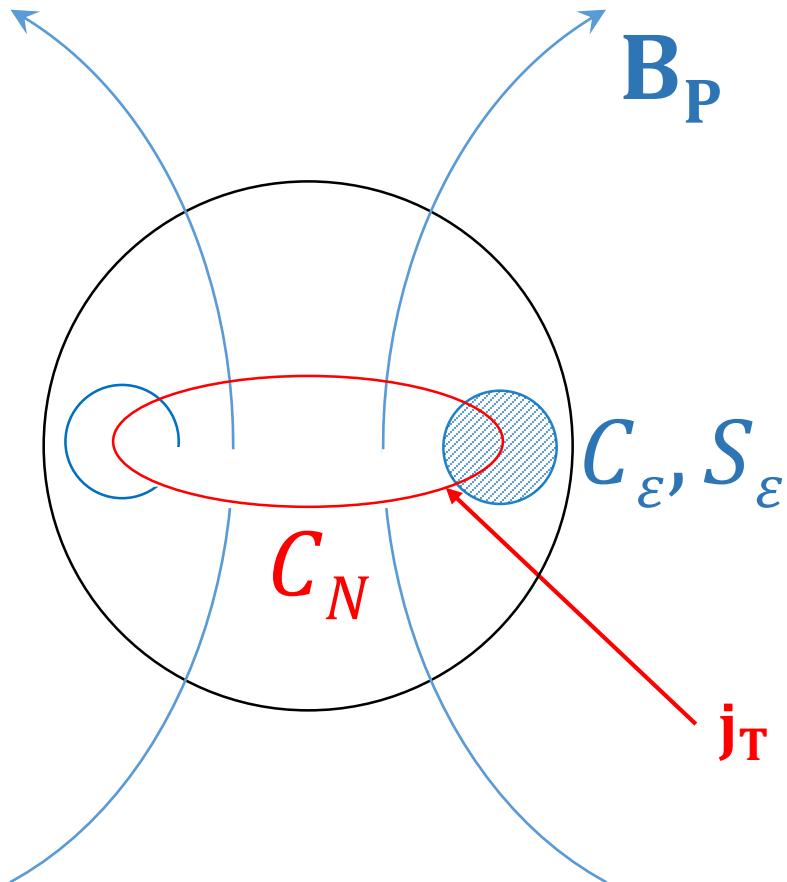
$$\Rightarrow \mathbf{j}_T = \mathbf{0} \text{ on } C_N$$

$$\Rightarrow \mathbf{B}_P = \mathbf{0}$$

Cowling's neutral point argument

Poloidal / Toroidal decomposition

$$\mathbf{j}_T = \nabla \times \frac{\mathbf{B}_P}{\mu} = \sigma(\mathbf{E}_T + \mathbf{u}_P \times \mathbf{B}_P)$$



Suppose σ is a tensor (anisotropic conductivity)

$$\mathbf{j}_T = [\sigma](\mathbf{E}_T + \mathbf{u}_P \times \mathbf{B}_P + \mathbf{E}_P + \mathbf{u}_T \times \mathbf{B}_P + \mathbf{u}_P \times \mathbf{B}_T)$$

\Rightarrow Cowling's neutral point argument fails



Anisotropic conductivity

Consider \mathbf{q} such that

$$\sigma = \begin{cases} \sigma^{\parallel} & \text{in the direction of } \mathbf{q} \\ \sigma^{\perp} & \text{in the directions } \mathbf{q}_1 \text{ and } \mathbf{q}_2, \text{ perpendicular to } \mathbf{q} \end{cases}$$

For example, in plasmas:

- $\sigma^{\parallel} = 1.96 \sigma^{\perp}$, with \mathbf{q} in the direction of the magnetic field

S. I. Braginskii, in *Reviews of Plasma Physics*, edited by M. A. Leontovich, Vol. 1
(Consultants Bureau, New York, 1965), pp.205–311.

Anisotropic conductivity

Consider a unit vector \mathbf{q} such that

$$\sigma = \begin{cases} \sigma^{\parallel} & \text{in the direction of } \mathbf{q} \\ \sigma^{\perp} & \text{in the directions } \mathbf{q}_1 \text{ and } \mathbf{q}_2, \text{ perpendicular to } \mathbf{q} \end{cases}$$

Look for $[\sigma_{ij}]$ satisfying $\mathbf{j} = [\sigma_{ij}] \mathbf{E}$, with

- If $\mathbf{E} = \mathbf{q}$ then $\mathbf{j} = \sigma^{\parallel} \mathbf{E} \Rightarrow [\sigma_{ij}] \mathbf{q} = \sigma^{\parallel} \mathbf{q}$
- If $\mathbf{E} \cdot \mathbf{q} = 0$ then $\mathbf{j} = \sigma^{\perp} \mathbf{E} \Rightarrow \begin{aligned} [\sigma_{ij}] \mathbf{q}_1 &= \sigma^{\perp} \mathbf{q}_1 \\ [\sigma_{ij}] \mathbf{q}_2 &= \sigma^{\perp} \mathbf{q}_2 \end{aligned}$

$$\Rightarrow \sigma_{ij} = \sigma^{\perp} \delta_{ij} + (\sigma^{\parallel} - \sigma^{\perp}) q_i q_j$$

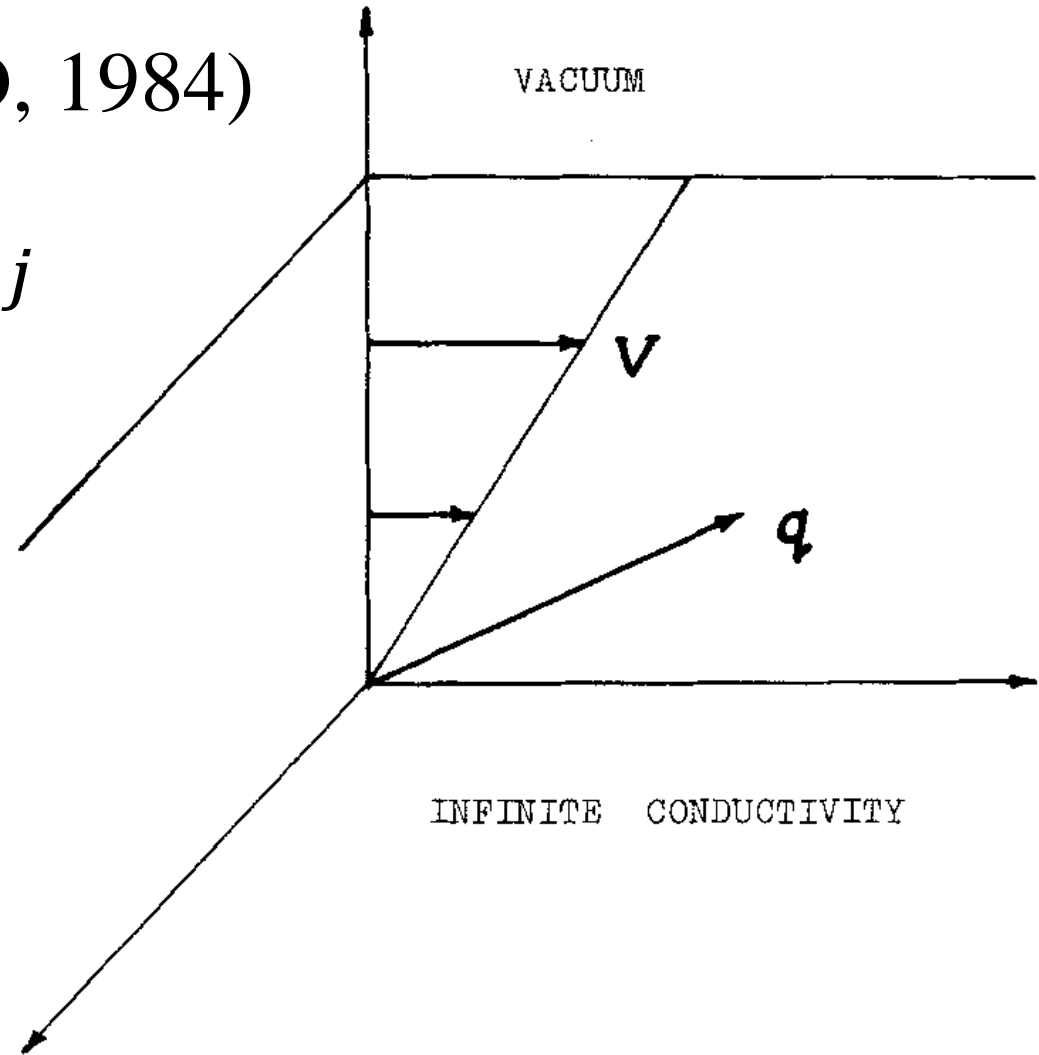
Other dynamo studies with anisotropic conductivity

Ruderman & Ruzmaikin (GAFD, 1984)

$$\sigma_{ij} = \sigma^{\perp} \delta_{ij} + (\sigma^{\parallel} - \sigma^{\perp}) q_i q_j$$

- Cartesian geometry
- Linear shear
- Asymptotic study

$$\sigma^{\perp} \gg \sigma^{\parallel}$$

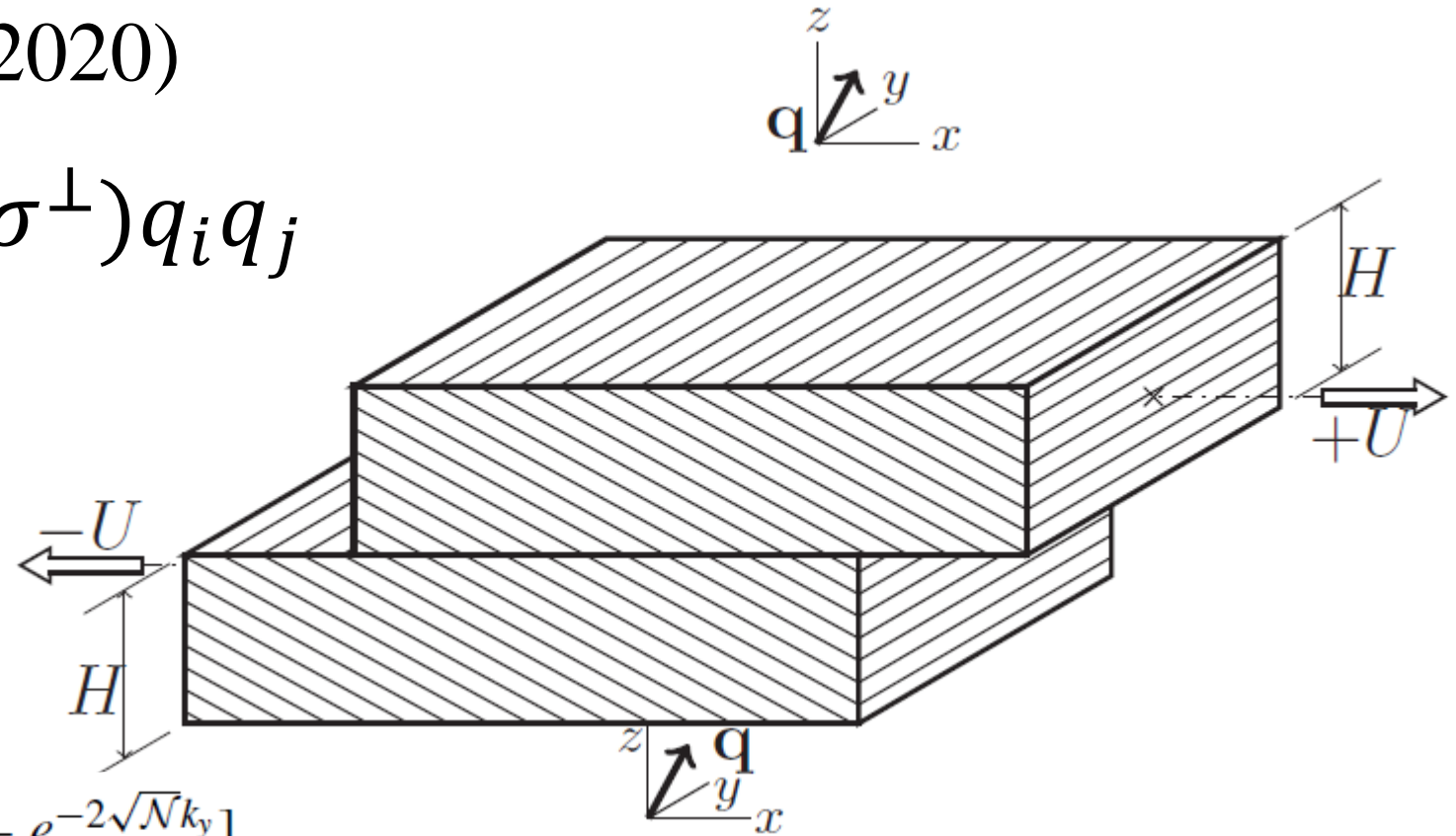


Other dynamo studies with anisotropic conductivity

Alboussière et al (PRE, 2020)

$$\sigma_{ij} = \sigma^\perp \delta_{ij} + (\sigma^\parallel - \sigma^\perp) q_i q_j$$

- Cartesian geometry
- Sliding plates
- Exact solutions



$$R_{mc} = \frac{k_y \mathcal{F}(\mathcal{N} - 1) [1 + e^{-2\sqrt{\mathcal{N}}k_y}]}{1 + e^{-2\sqrt{\mathcal{N}}k_y} \left[1 + \frac{1}{\sqrt{\mathcal{N}}}\right] - \frac{1}{\sqrt{\mathcal{N}}} - 2e^{-(1+\sqrt{\mathcal{N}})k_y}}.$$

Other dynamo studies with anisotropic conductivity

Lortz (Z. Naturforsch, 1989)

$$[\sigma] = \begin{pmatrix} 1 & 0 & 0 \\ 2 & 1 & e \\ 0 & e & 1 \end{pmatrix}_{(\mathbf{e}_r, \mathbf{e}_\theta, \mathbf{e}_z)}$$

- Torus geometry
- Asymptotic study in the limit of zero torus curvature
- Formal proof, without specifying any velocity field.

Logarithmic spiral anisotropy

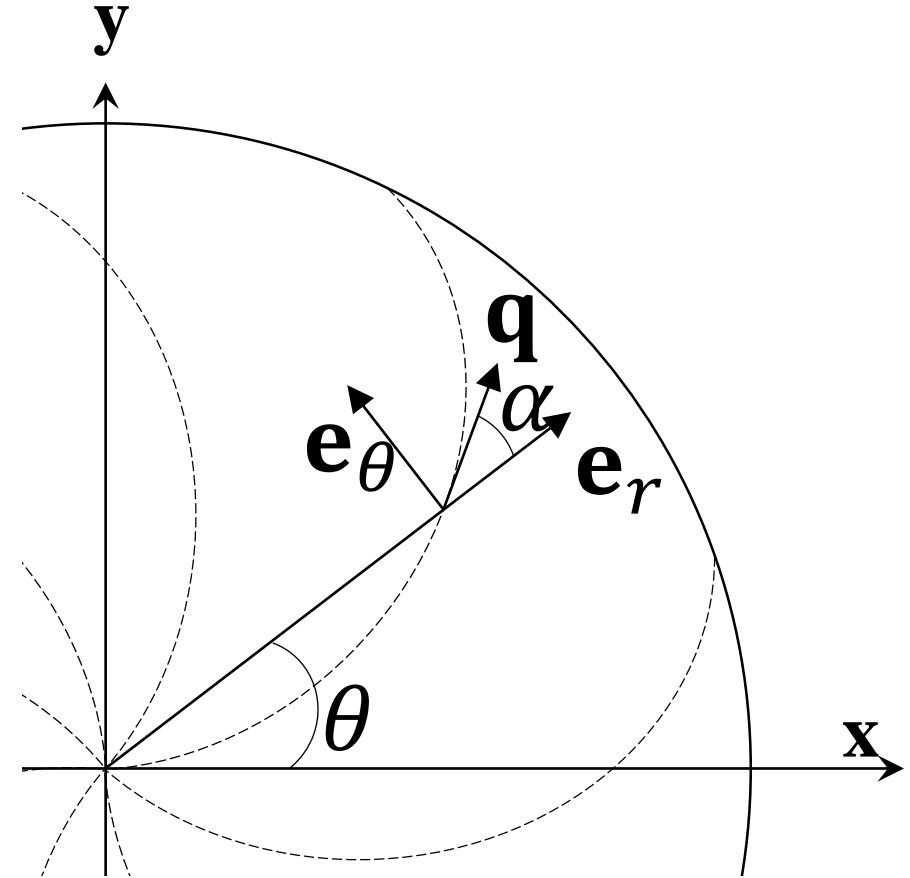
We choose a logarithmic spiral anisotropy

$$\mathbf{q} = \cos \alpha \mathbf{e}_r + \sin \alpha \mathbf{e}_\theta$$

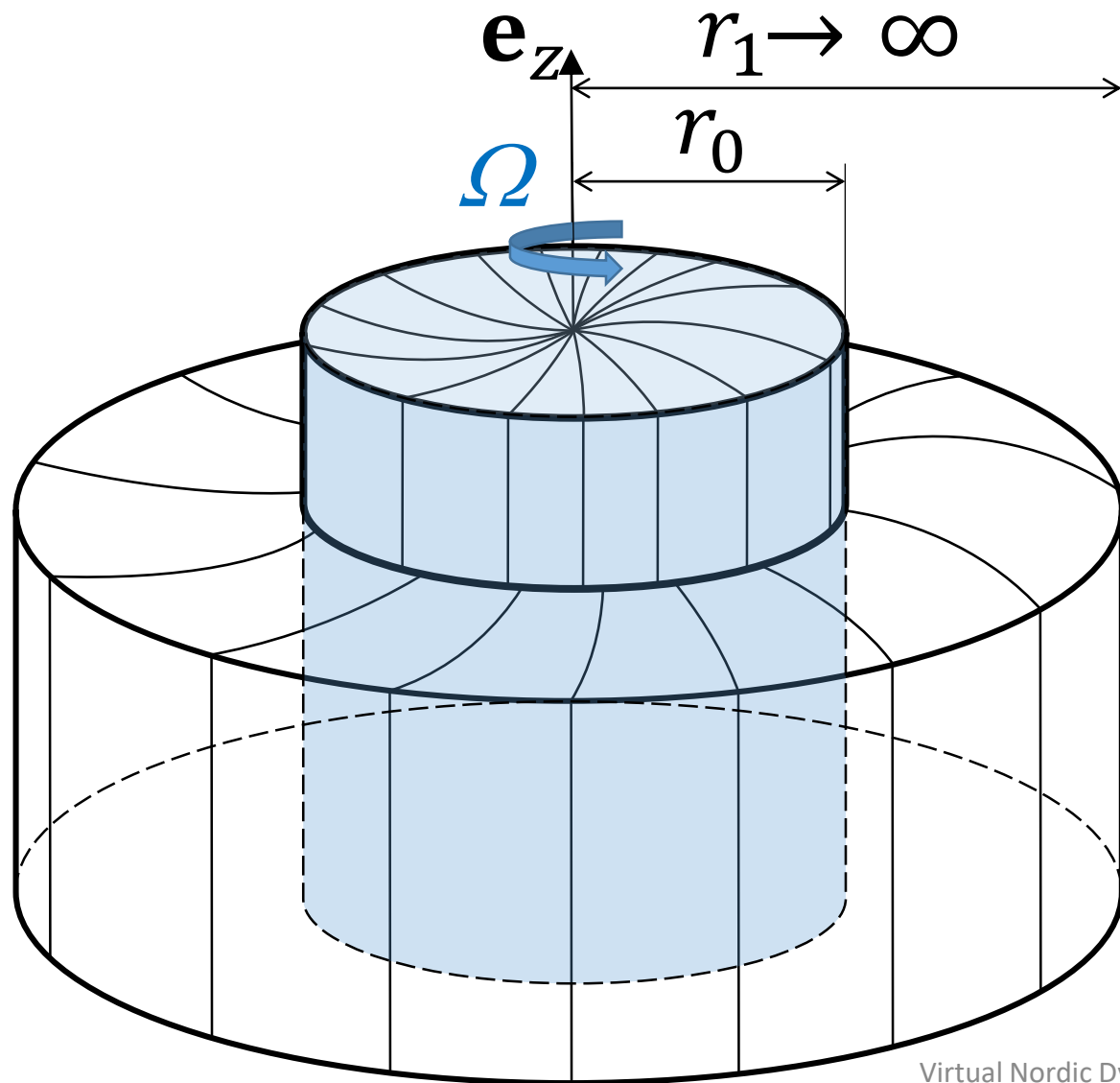
$$[\sigma] = \begin{pmatrix} \sigma^\parallel c^2 + \sigma^\perp s^2 & (\sigma^\parallel - \sigma^\perp)cs & 0 \\ (\sigma^\parallel - \sigma^\perp)cs & \sigma^\parallel s^2 + \sigma^\perp c^2 & 0 \\ 0 & 0 & \sigma^\perp \end{pmatrix}$$

$(\mathbf{e}_r, \mathbf{e}_\theta, \mathbf{e}_z)$

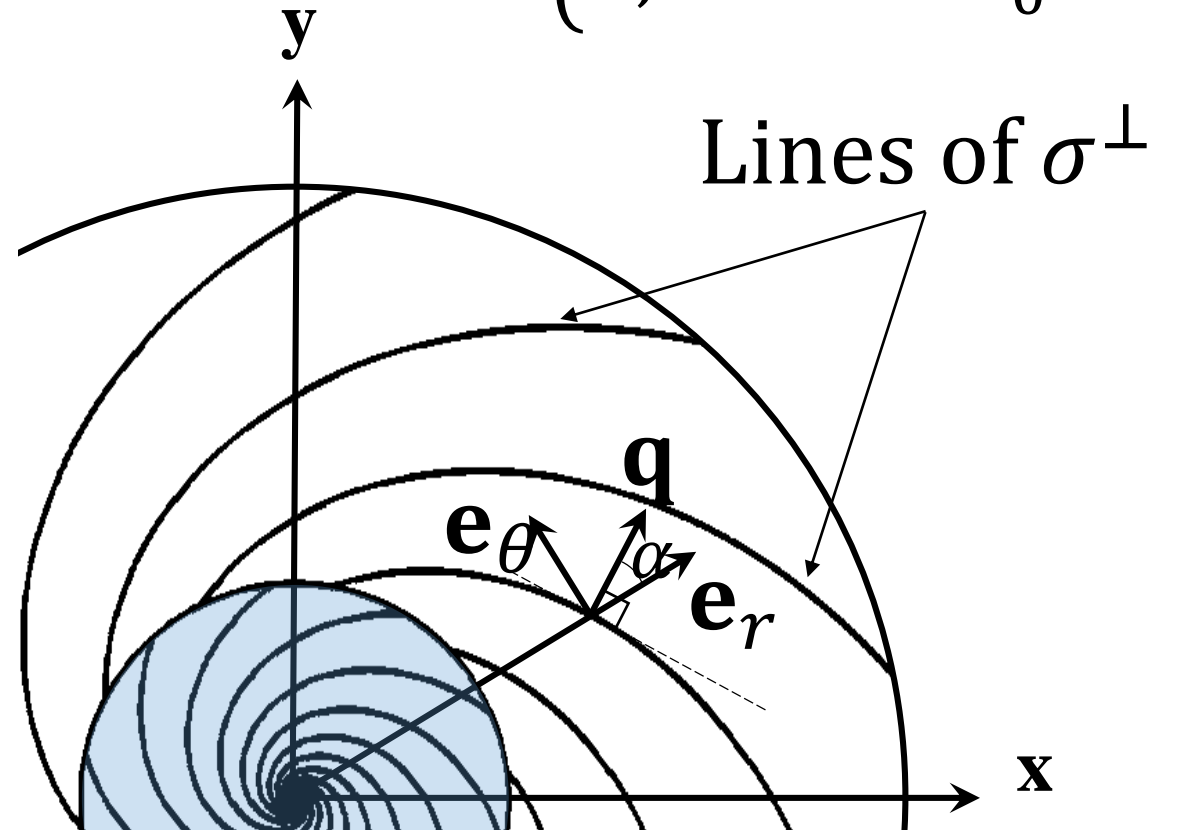
$$(c, s) = (\cos \alpha, \sin \alpha)$$



Inner cylinder in solid body rotation



$$\mathbf{u} = \begin{cases} r\Omega\mathbf{e}_\theta, & r \leq r_0 \\ \mathbf{0}, & r > r_0 \end{cases}$$




1. How can anisotropic conductivity beat Cowling's antidynamo theorem ?
2. **Exact solution of the induction equation**
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Dimensionless equations

Induction equation $\partial_t \mathbf{B} = \nabla \times (\mathbf{u} \times \mathbf{B}) - \nabla \times ([\eta] \nabla \times \mathbf{B})$

Anisotropic diffusivity $\eta_{ij} = \delta_{ij} + \eta_1 q_i q_j, \quad \eta_1 = \frac{\sigma^\perp}{\sigma^\parallel} - 1$

Solid body rotation $\mathbf{u} = \begin{cases} r\Omega \mathbf{e}_\theta, & r \leq 1 \\ \mathbf{0}, & r > 1 \end{cases} \Rightarrow \nabla \times (\mathbf{u} \times \mathbf{B}) = 0$

Axisymmetry $\mathbf{B}(r, z, t) = \tilde{B} \mathbf{e}_\theta + \nabla \times (\tilde{A} \mathbf{e}_\theta)$ 

Stationary and z-independent flow conjugated to linearity of Ind. Eq. implies

$$\mathbf{B} = \left(-ikA, B, \frac{1}{r} \partial_r (rA) \right) \exp(\gamma t + ikz) \Rightarrow \text{1D problem}$$

Resolution

$$\mathbf{B} = \left(-ikA, B, \frac{1}{r} \partial_r (rA) \right) \exp(\gamma t + ikz)$$

$$\gamma A + D_k(A) = i\eta_1 cskB - \eta_1 s^2 D_k(A),$$

$$\gamma B + D_k(B) = -i\eta_1 cskD_k(A) - \eta_1 c^2 k^2 B,$$

$$\eta_1 = \frac{\sigma^\perp}{\sigma^\parallel} - 1$$

where $D_\nu(X) = \nu^2 X - \partial_r[\frac{1}{r} \partial_r (rX)]$, $c = \cos \alpha$ and $s = \sin \alpha$.

Looking for the dynamo threshold ($\gamma = 0$) leads to

$$D_{\tilde{k}}(B) = D_k \left(B - i \frac{ck}{s} A \right) = 0, \quad \tilde{k} = k \left(\frac{1 + \eta_1}{1 + \eta_1 s^2} \right)^{1/2}$$

Solution at threshold

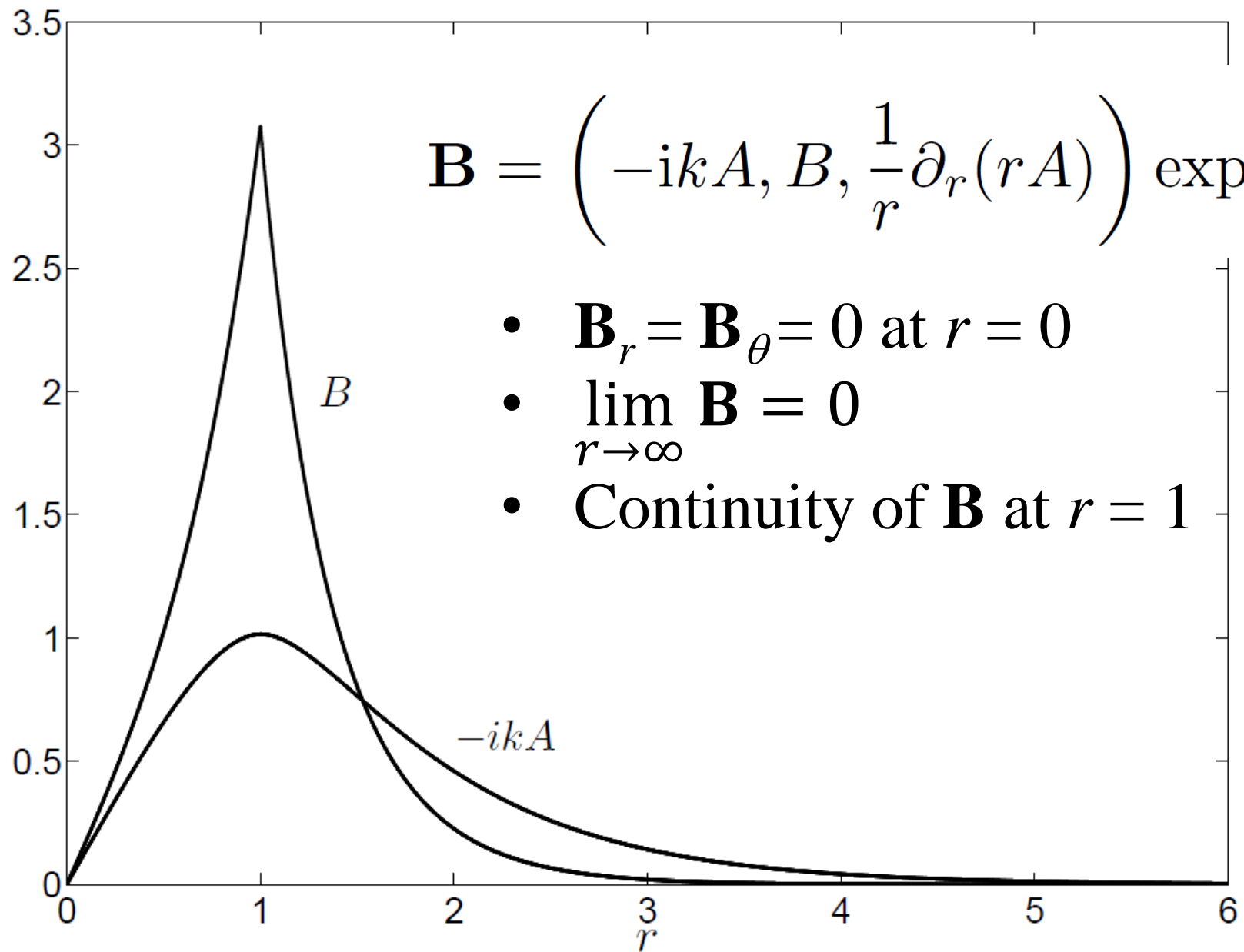
The solutions of $D_\nu(X) = 0$ being a linear combination of $I_1(\nu r)$ and $K_1(\nu r)$, we find

$$r < 1, \quad \begin{cases} A = \frac{s}{ick} \left(\lambda \frac{I_1(\tilde{k}r)}{I_1(\tilde{k})} + \mu \frac{I_1(kr)}{I_1(k)} \right) \\ B = \lambda \frac{I_1(\tilde{k}r)}{I_1(\tilde{k})} \end{cases} \quad (13)$$

$$r > 1, \quad \begin{cases} A = \frac{s}{ick} \left(\lambda \frac{K_1(\tilde{k}r)}{K_1(\tilde{k})} + \mu \frac{K_1(kr)}{K_1(k)} \right) \\ B = \lambda \frac{K_1(\tilde{k}r)}{K_1(\tilde{k})}, \end{cases} \quad (14)$$

$$\text{with } \lambda \Gamma(\tilde{k}) + \mu \Gamma(k) = 0$$

where I_1 and K_1 are modified Bessel functions of first and second kind. In (13) and (14) the following boundary conditions have been applied to A and B : finite values at $r = 0$, continuity at $r = 1$, and $\lim_{r \rightarrow \infty} A, B = 0$.



A crucial boundary condition

The continuity of \mathbf{E}_z implies the following identity

$$(\partial_r B - ik\Omega A)(r = 1^-) = \partial_r B(r = 1^+).$$

Here is the velocity!



It corresponds to the differential rotation
between the inner and outer cylinders

A crucial boundary condition

The continuity of \mathbf{E}_z implies the following identity

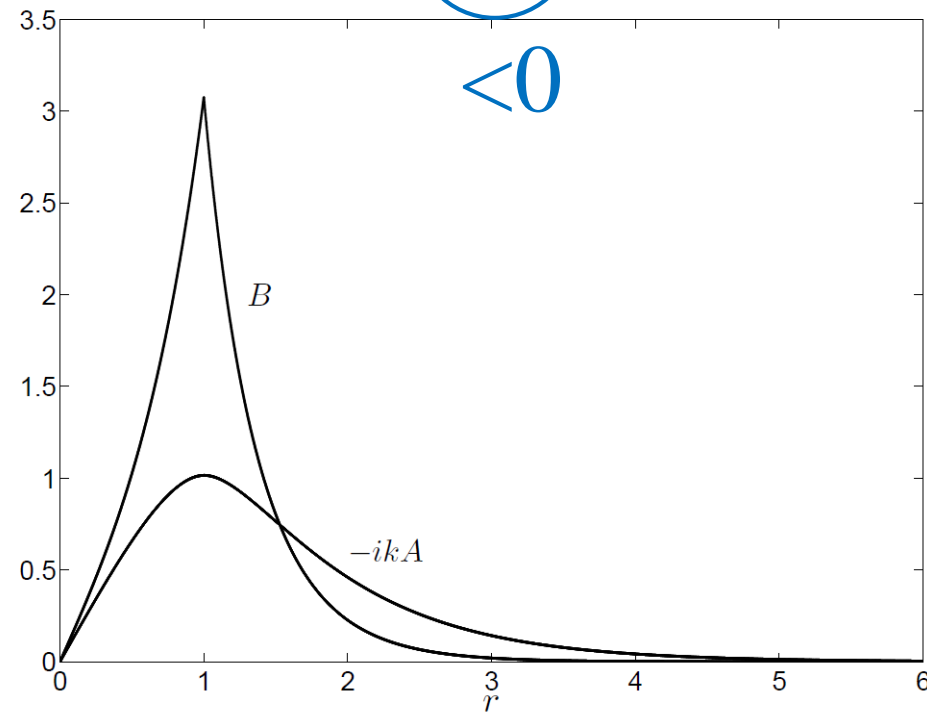
$$(\partial_r B - ik\Omega A)(r = 1^-) = \partial_r B(r = 1^+).$$

>0

>0

<0

$\Rightarrow \Omega < 0$



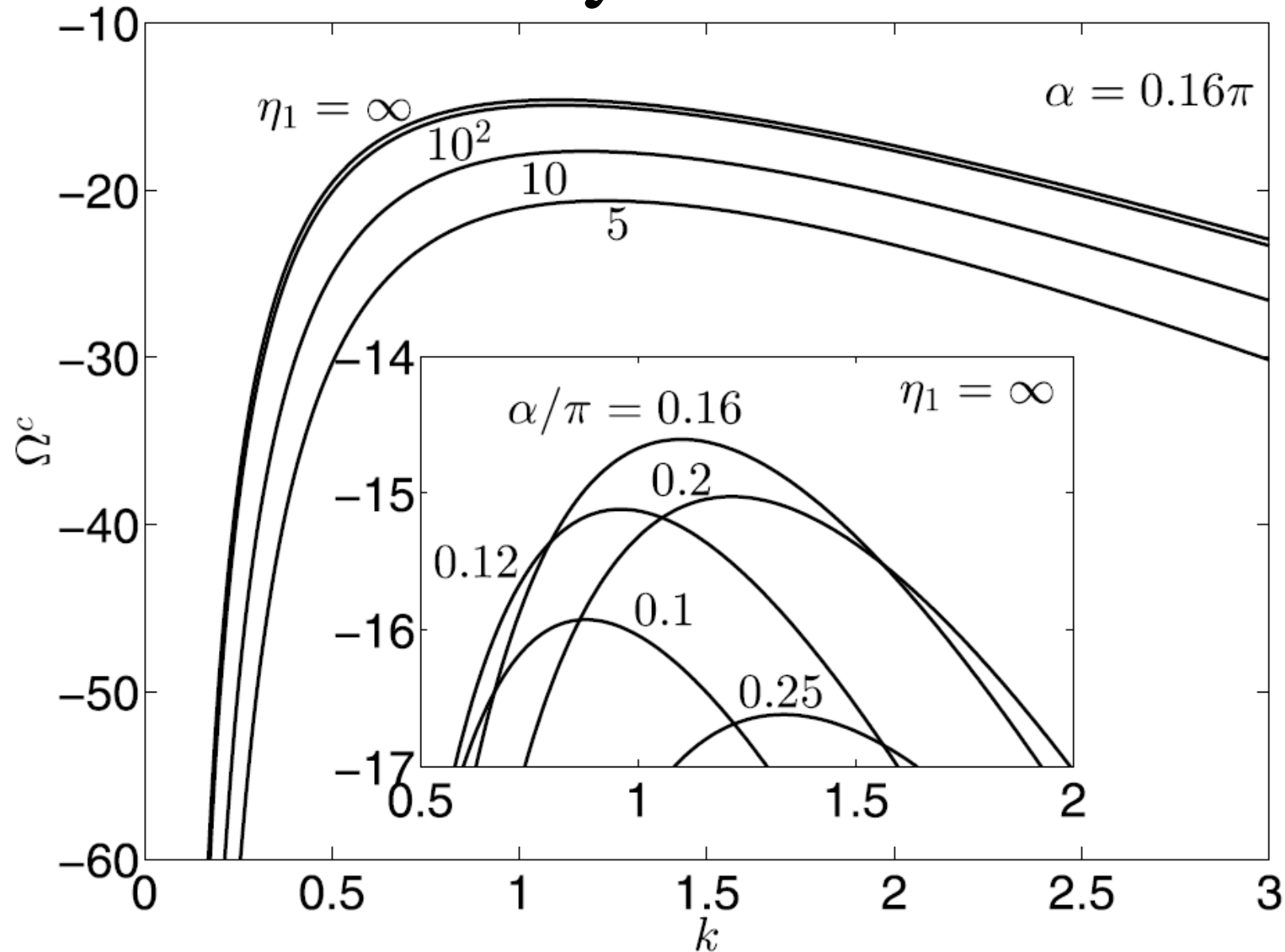
Dynamo threshold

$$\Omega^c = \frac{c}{s} (I_1(\tilde{k})K_1(\tilde{k}) - I_1(k)K_1(k))^{-1}$$

Explicit  expression !

with $\tilde{k} = k \left(\frac{1 + \eta_1}{1 + \eta_1 s^2} \right)^{1/2}$ $\eta_1 = \frac{\sigma^\perp}{\sigma^\parallel} - 1$

Dynamo threshold



$$\sigma^\perp > \sigma^\parallel$$

$$\eta_1 = \frac{\sigma^\perp}{\sigma^\parallel} - 1 > 0$$

Dynamo threshold

The minimum value of $|\Omega^c|$ is obtained for $\eta_1 \rightarrow \infty$,
 $k^* = 1.1$ and $\alpha^* = 0.16\pi$,

$$\Omega^* = \min_{\eta, k, \alpha} |\Omega^c| = 14.6$$

results. Considering an inner cylinder of radius $r_0 = 0.05$ m, taking the conductivity of copper $\mu_0\sigma_0 \approx 72.9$ s m⁻² leads to a dynamo threshold $f^* = \Omega^*(2\pi\mu_0\sigma_0r_0^2)^{-1} \approx 12.8$ Hz. Provided the cylinder height and outer radius r_1 are sufficiently large, this is experimentally achievable. Such an anisotropic

⇒ experimentally feasible



Understanding

Crucial term

$$\gamma \mathbf{B}_r = \eta_1 c s k^2 \mathbf{B}_\theta - (1 + \eta_1 s^2) D_k(\mathbf{B}_r),$$

$$\gamma \mathbf{B}_\theta = \eta_1 c s D_k(\mathbf{B}_r) - (D_k + \eta_1 c^2 k^2) \mathbf{B}_\theta + \frac{s}{c} (\partial_r \Omega) \mathbf{B}_r$$

Diffusive terms

Differential rotation

$$\eta = \begin{pmatrix} 1 + \eta_1 c^2 & \eta_1 c s & 0 \\ \eta_1 c s & 1 + \eta_1 s^2 & 0 \\ 0 & 0 & 1 \end{pmatrix}$$

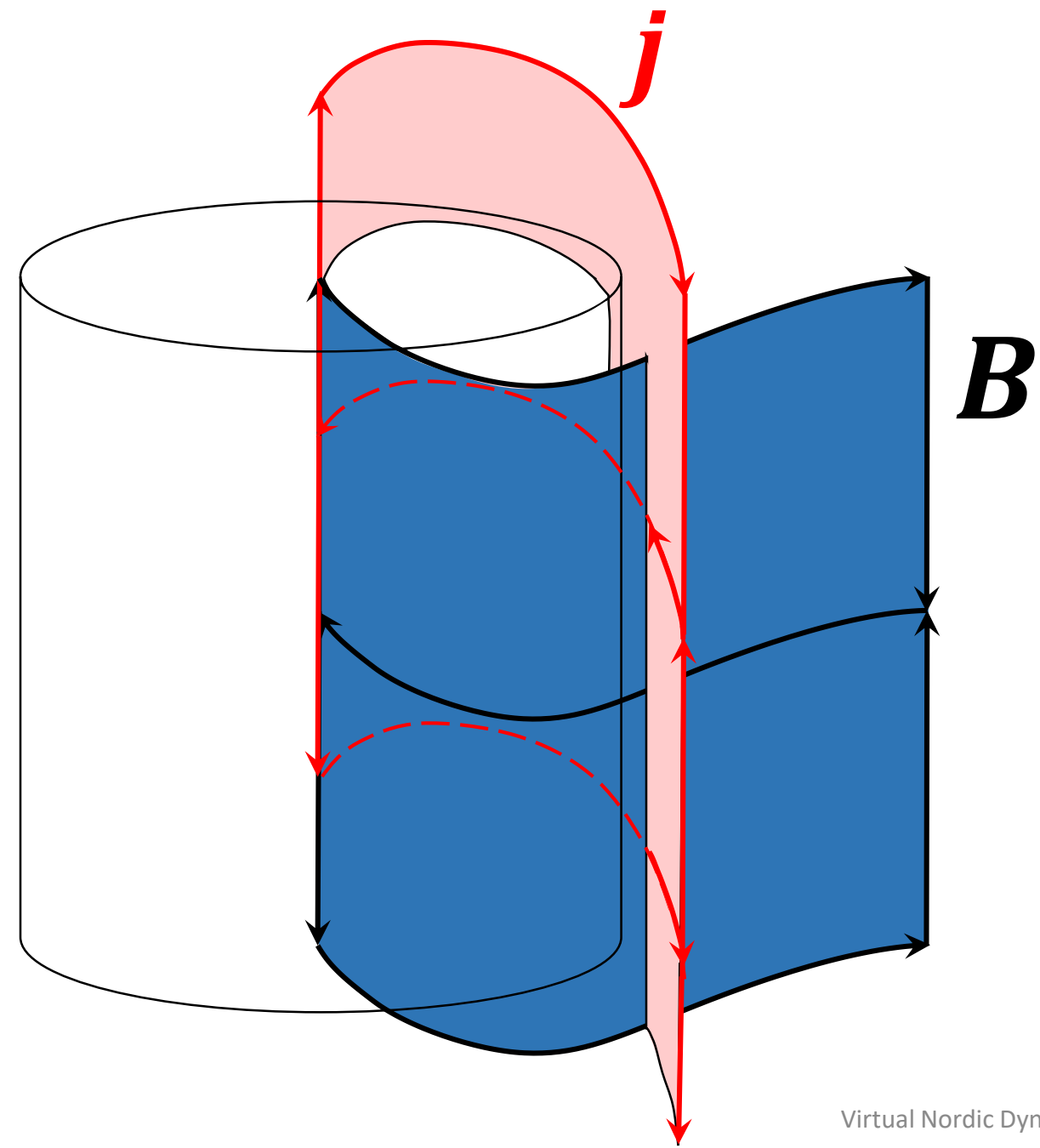
Spiraling currents

$$\mathbf{B} = \left(-ikA, B, \frac{1}{r} \partial_r(rA) \right) \exp(\gamma t + ikz)$$

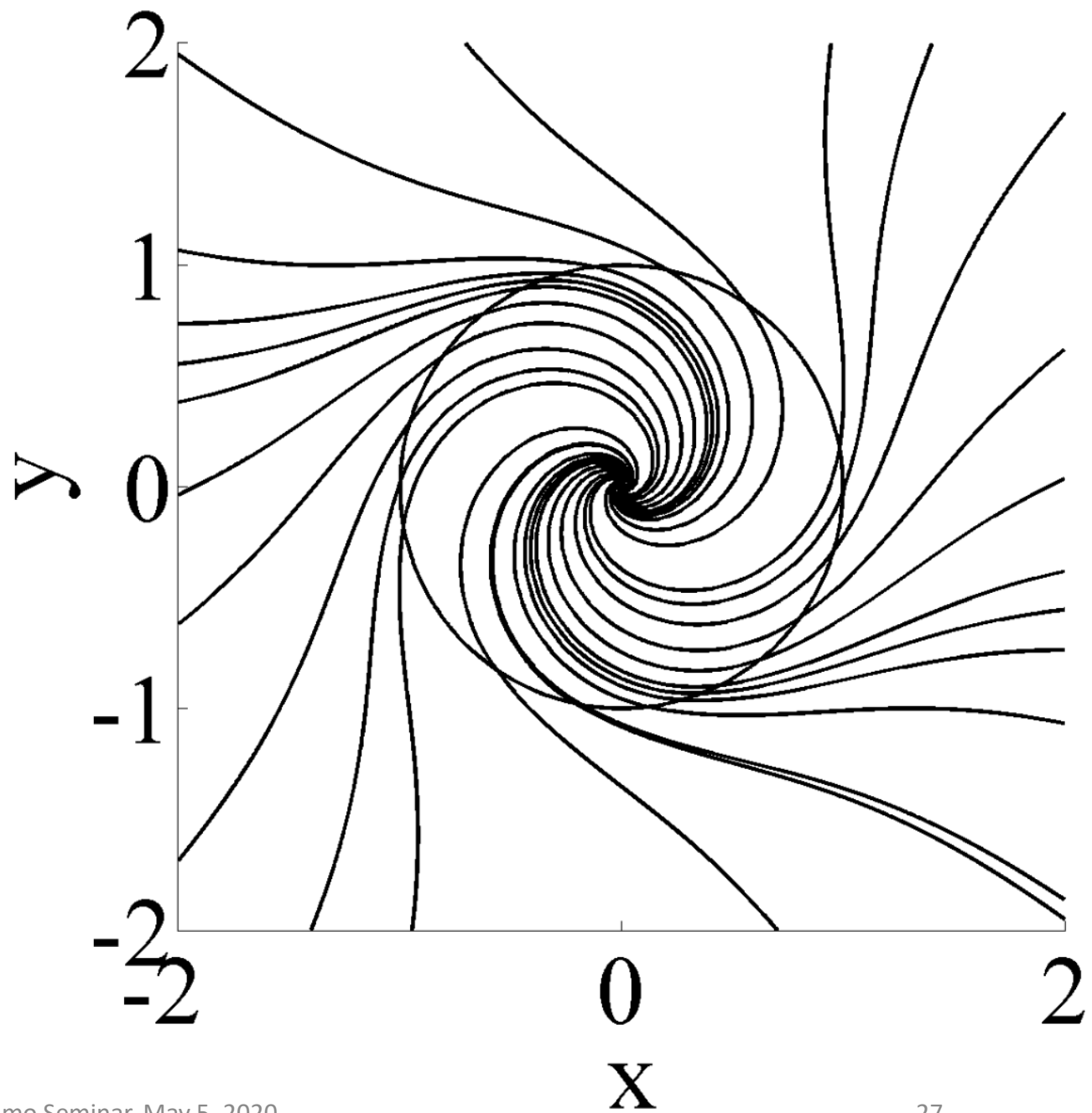
$$\mathbf{j} = \left(-ikB, D_k(A), \frac{1}{r} \partial_r(rB) \right) \exp(\gamma t + ikz)$$

$$\text{At threshold: } \frac{j_\theta}{j_r} = -\frac{\eta_1 c s}{1 + \eta_1 s^2} \Rightarrow \text{spiraling currents}$$

$$\eta_1 \rightarrow \infty \Rightarrow \mathbf{j} \cdot \mathbf{q} = 0$$



B



1. How can anisotropic conductivity beat Cowling's antidynamo theorem ?
2. Exact solution of the induction equation
3. **Conclusion and outlook**

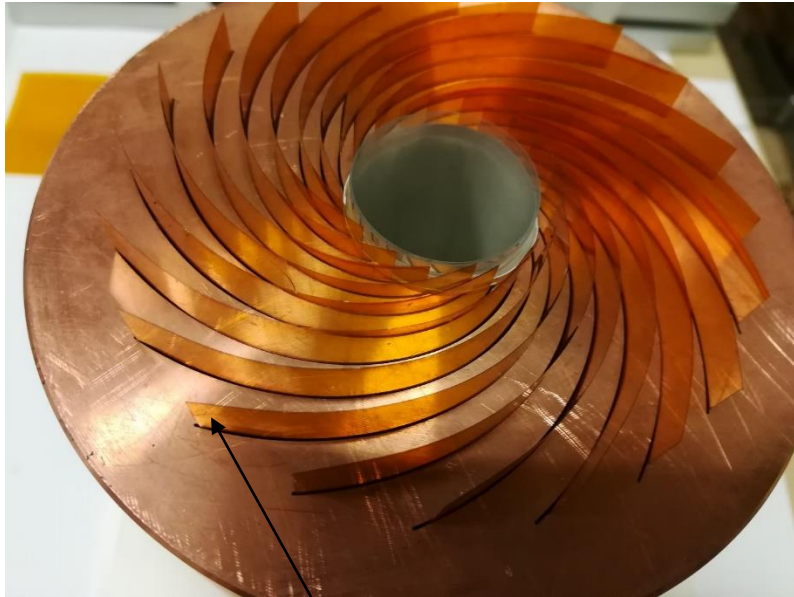
Conclusion and outlook

- **Axisymmetric dynamo** action is possible with anisotropic conductivity
- **Exact solution** for logarithmic spiral anisotropy and simple azimuthal shear
- Threshold sufficiently low to be **experimentally achievable**
- Application to plasmas ?

An experimental demonstration

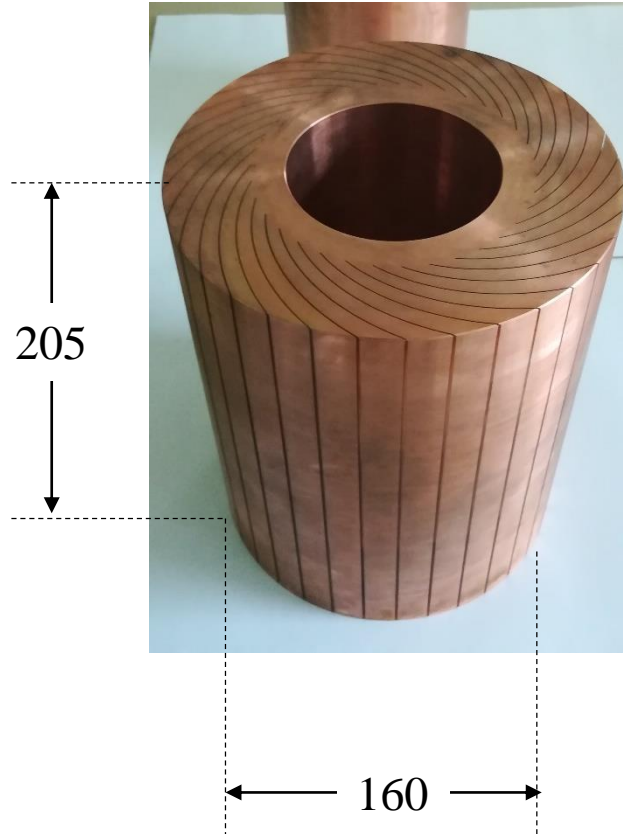
$$\sigma^{\perp} > \sigma^{\parallel}$$

Inner cylinder



Spiraling insulator
(kapton + epoxy)

Outer cylinder



Both cylinders before
final electroerosion



Application to plasmas ?

where the electrical conductivities are

$$\sigma_{\perp} = \frac{e^2 n_e \tau_e}{m_e} = \sigma_1 T_e^{3/2},$$

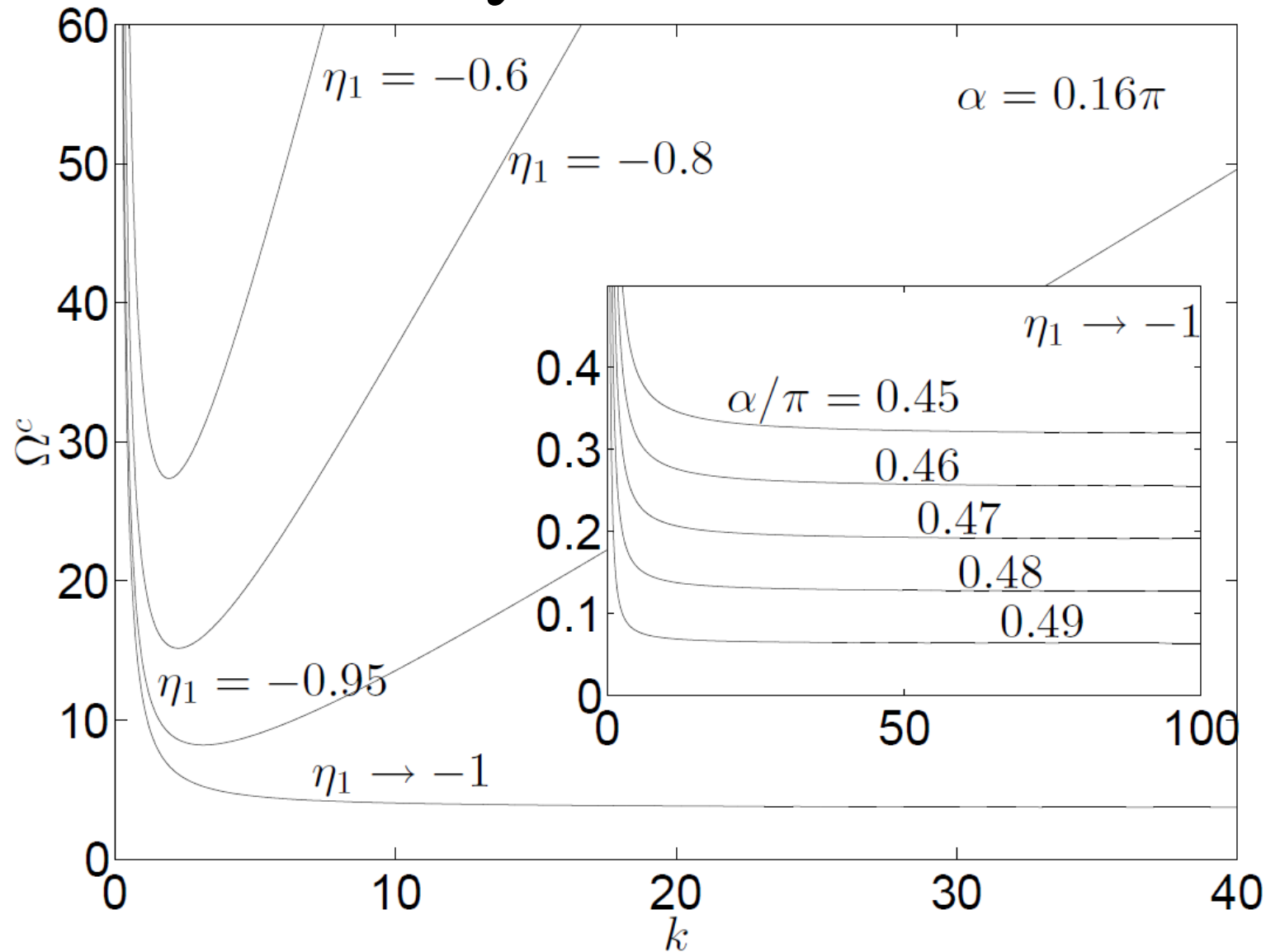
$$\sigma_{\parallel} = 1.96 \sigma_{\perp} = 1.96 \sigma_1 T_e^{3/2},$$

$$\eta_1 \sim -0,5$$

- S. I. Braginskii, in *Reviews of Plasma Physics*, edited by M. A. Leontovich, Vol. 1 (Consultants Bureau, New York, 1965), pp.205–311.

$$\sigma^{\perp} < \sigma^{\parallel} \Rightarrow \eta_1 = \frac{\sigma^{\perp}}{\sigma^{\parallel}} - 1 < 0$$

Dynamo threshold



$$\sigma^\perp < \sigma^\parallel$$

$$\eta_1 = \frac{\sigma^\perp}{\sigma^\parallel} - 1 < 0$$